



VTEC Laboratories Inc.

April 29, 2011

Mr. Keene Christopher
Airkrete, Inc.
PO Box 380
Weedsport, NY 13166

Subject: Standard Test Method For Thermal Conductivity
According to ASTM C 518.

Job #: 100-3783


Tested: April 29, 2011

Sample Description: Aircrete Greensulation

RESULTS:

Sample Thickness	Hot Face Temp	Cold Face Temp	Average Temp	Thermal Conductivity	Total Thermal Resistance	Thermal Resistance per inch
inch	Deg F	Deg F	Deg F	BTU·in/hr·ft ² ·F°	hr·ft ² ·F°/BTU	hr·ft ² ·F°/BTU·in
3.4	78.26	66.68	72.47	0.285	11.93	3.51

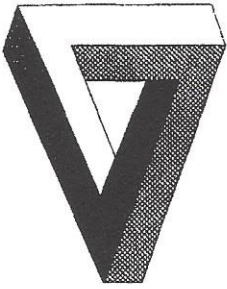
NOTE: Specimen had several cracks and those were closed by applying side pressure to the samples.


Neil Schultz
Executive Director


Amirudin Rahim
Technical Director

DISCLAIMER: This test result alone does not assess the fire hazard of the material, or a product made from this material, under actual fire conditions. Consequently, the results of this test alone are not to be quoted in support of claims with respect to the fire hazard of the material or product under actual fire conditions. The results when used alone are only to be used for research and development, quality control and material specifications.

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VTEC Laboratories Inc.

November 21, 2011

Mr. Keene Christopher
Airkrete, Inc.
PO Box 380
Weedsport, NY 13166

Subject: Standard Test Method For Thermal Conductivity
According to ASTM C 518.

Job #: 100-3783-2

Tested: November 19, 2011

Sample Description: Aircrete Greensulation

RESULTS:

Sample Thickness	Hot Face Temp	Cold Face Temp	Average Temp	Thermal Conductivity	Total Thermal Resistance	Thermal Resistance per inch
inch	Deg F	Deg F	Deg F	BTU·in/hr·ft ² ·F°	hr·ft ² ·F°/BTU	hr·ft ² ·F°/BTU·in
3.5	77.23	66.95	72.09	0.321	10.89	3.11

NOTE: Specimen had several cracks that were closed by applying side pressure to the samples and gaps were filled with smaller pieces and powder.


Neil Schultz
Executive Director


Amirudin Rahim
Technical Director

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HOLOMETRIX, INC.

Report on

THE APPARENT THERMAL CONDUCTIVITY AND THERMAL RESISTANCE OF
A SPECIMEN OF A CELLULAR INSULATION MATERIAL

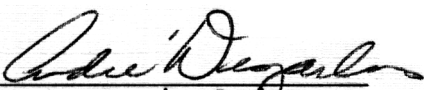
Prepared for:

Air Krete, Inc.
East Brutus Street
Weedsport, NY 13166

Holometrix Report Number CLR-7

Work Performed Under Purchase Order Number 0439

Submitted by:



A. O. Desjarlais
Manager
Thermal Insulation Evaluation
Thermophysics Laboratory

May 1989

HOLOMETRIX, INC.

Report on

THE APPARENT THERMAL CONDUCTIVITY AND THERMAL RESISTANCE OF A SPECIMEN OF A CELLULAR INSULATION MATERIAL

A specimen of a cellular insulation material was submitted for the analysis of apparent thermal conductivity and thermal resistance of 2C (35F). The specimen was identified as Air-Krete Insulation and a sample approximately dimensioned 290mm (11.5 inches) square by 50.1mm (2.01 inches) thick was supplied. This sample had a test density of 82.2 Kg m⁻³ (5.13 lbs ft⁻³).

HOLOMETRIX, INC.

Experimental Procedure for Testing by ASTM C518-85 (Rapid-k)

Each specimen was evaluated in accordance with ASTM C518-85, "Steady-State Heat Flux Measurements and Thermal Transmission Properties by Means of the Heat Flow Meter Apparatus" utilizing a Holometrix Model Rapid-k heat flow meter instrument. A schematic diagram of the test facility is shown in Figure 1. The specimen was installed horizontally between 300 mm (12 inch) square aluminum surface plates treated to have a total hemispherical emittance of 0.82 at 24C (75F). The surface plates were smoothly finished to conform to a true plane within a 0.25 percent. Above the upper (hot) and below the lower (cold) surface plates, heaters, heat sinks and insulation were installed. The two heat sink assemblies were connected to a refrigeration system capable of maintaining -30C (-20F) at the heat sink. Temperature control of the surface plates was accomplished by operating the refrigeration system continuously and reheating with the electrical resistance heaters. The temperatures of the surface plates were controlled and monitored by temperature sensors mounted near the heaters and in the surface plates.

Between the bottom of the test specimen and the bottom surface plate, a heat flux transducer was installed. The instrument heat flux transducer utilized has a sensing area 100 mm (4 inches) square located in the center of its 300 mm (12 inch) square overall area.

Temperature measurements were performed by utilizing Type T Copper/Constantan thermocouples calibrated to the special limits of error specified in ASTM E230-83, "Temperature-Electromotive Force (EMF) Tables for Standardized

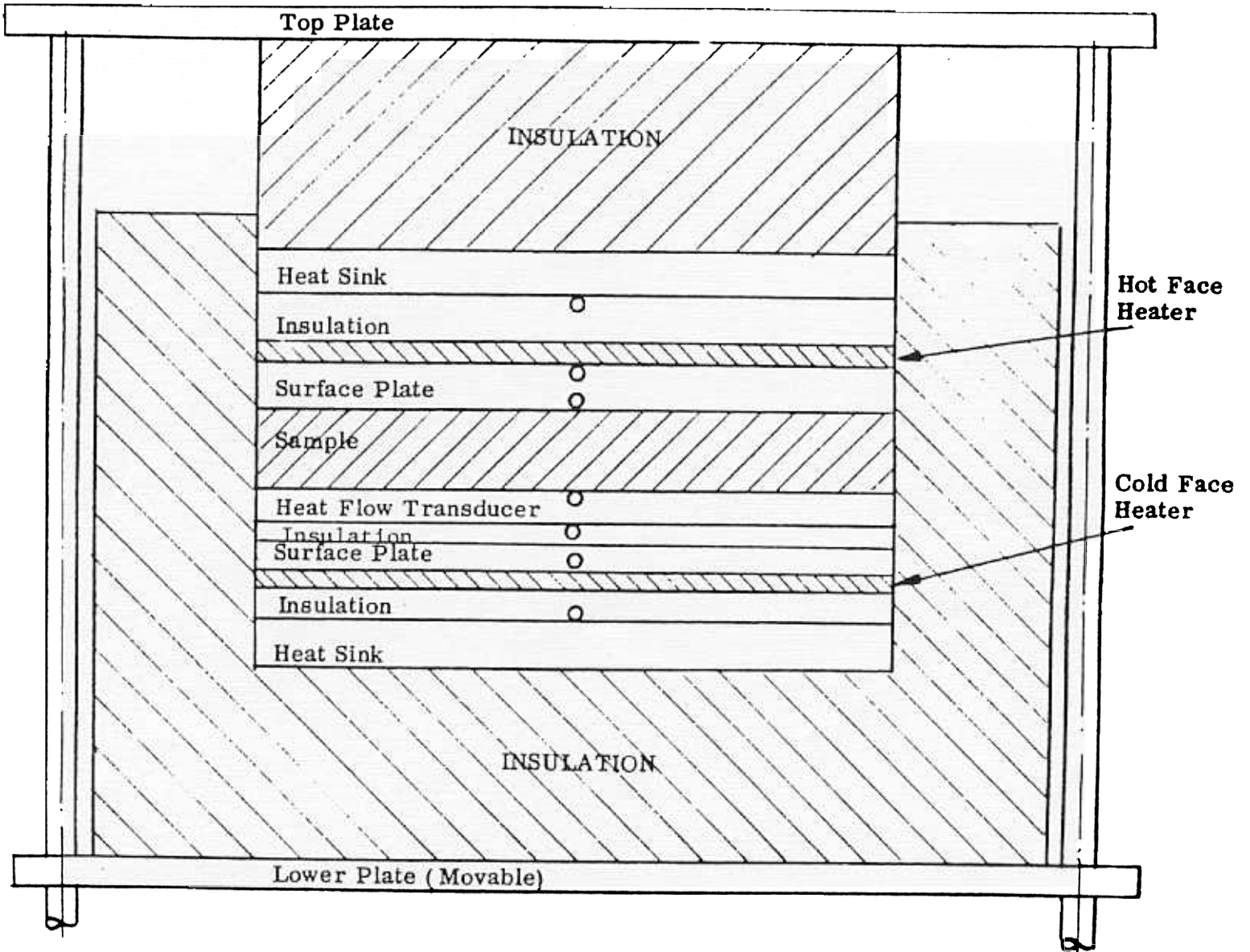


Figure 1

SCHMATIC OF HEAT FLOW METER
THERMAL CONDUCTIVITY INSTRUMENT

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Thermocouples." All thermocouple sensors were fabricated with No. 30 AWG wire. Single temperature sensors were used for measuring the hot and cold surface plate temperatures in the center of the sensing area of the instrument heat flux transducer. All temperature sensors were individually connected to a digital millivolt meter having a resolution of ± 1 microvolt.

The bottom surface plate assembly could be adjusted to accommodate surface plate separations from 0 to 100 mm (0 to 4 inches). The opening between the surface plates was measured by using a linear motion potentiometer. The periphery of the test stack was lined with 50 mm (2 inches) of an extruded polystyrene foam insulation having a thermal resistance of about $1.8 \text{ m}^2\text{K/W}$ ($10 \text{ hr ft}^2 \text{ F/Btu}$) at 24C (75F).

In operation, the plate separation was adjusted to accommodate the test thickness of the specimen being evaluated. Typically the thickness of the specimen was measured prior to its insertion into the instrument and the plates were closed such that the thickness readout corresponded to the average test specimen thickness. The temperature of the top and bottom surface plates were adjusted such that the mean temperature and temperature difference test requirements were satisfied. If no temperature difference requirements were given, 28C (50F) was used.

At equilibrium, established after ensuring that during five consecutive observations at intervals of approximately 1200 seconds the test specimen apparent thermal conductivity changed less than 1 percent and not monotonically, the temperatures of both hot and cold faces were evaluated from

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the sensors embedded in the plates, and the heat flux through the specimen was derived from the heat flux transducer output.

The test specimen apparent thermal conductivity was calculated from

$$K = \frac{(S_I) (HFTOP)_I dX}{dT}$$

and the thermal resistance was calculated from

$$R = dx/K,$$

where

- K = test specimen apparent thermal conductivity;
- S_I = instrument heat flux transducer sensitivity;
- $HFTOP_I$ = instrument heat flux transducer output;
- dX = test specimen thickness; and
- dT = temperature difference across test specimen ; and
- R = thermal resistance

The instrumentation was calibrated using the National Bureau of Standards' Standard Reference Material 1450b. The calibration specimen is a high density fibrous glass material, 1.0 inches thick, having a thermal resistance of approximately 4.2 hr ft² F/Btu. The instrumentation was calibrated before and after every change in the surface plate temperatures.

results are summarized in the following tables.

TABLE 1

THE APPARENT THERMAL CONDUCTIVITY AND THERMAL RESISTANCE
OF A SPECIMEN OF A CELLULAR INSULATION MATERIAL

Specimen	Test Thickness	Test Density	Mean		W/m K	Btu-in/hr ft ² F	Thermal Resistance		
			mm	inches				kg/m ³	lbs/ft ³
Air-Krete	50.1	1.97	82.2	5.13	2	35	0.0378	0.262	7.53